# Anion Exchange Separation of Hard Acid-metals Using HF-H<sub>3</sub>BO<sub>3</sub> Media

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Takeo Adachi

Analytical Chemistry Laboratory, Japan Atomic Energy Research Institute, Tokai, Ibaraki 319-11 (Received October 2, 1981)

The properties of HF-H<sub>3</sub>BO<sub>3</sub> media and the distribution coefficients of eighteen metals have been investigated to achieve the separation of hard acid-metals by the anion exchange method. As the addition of boric acid to hydrofluoric acid solution reduces the free fluoride ion concentration to about one hundredth, it is possible to control the formation of metal fluoride complexes in a way favorable for the separation. The BF<sub>4</sub><sup>-</sup> and BF<sub>3</sub>OH-produced in this media are adsorbed strongly to the resin and reduce the relative adsorbabilities of metal fluoride complexes remarkably. Using these properties of HF-H<sub>3</sub>BO<sub>3</sub> media and the adsorbabilities of other anions, a new anion exchange method for the separation of hard acid-metals has been proposed. The new method is especially useful for the separation of titanium, zirconium, niobium, and tantalum. Distribution coefficients and elution behaviors of metal ions are not affected by the increase of the amount of metals because of the buffer action relating to the fluoride ion in HF-H<sub>3</sub>BO<sub>3</sub> media.

Most ion exchange separations of hard acid-metals<sup>1)</sup> such as titanium, zirconium, niobium, tantalum, tungsten, molybdenum, and tin have been done using anion exchange resins<sup>2)</sup> (unless otherwise devised<sup>3)</sup>), because these metals are easily hydrolysed in the absence of complexing agents and tend to form stable anion complexes in the presence of complexing agents.

As anion complexes of these metals have similar chemical properties, the separation of these metals is not easy, and many efforts have been attempted. 4-13) The following three points are considered to be essential for the satisfactory separation:

- (1) Select a proper complexing agent forming metal complexes whose chemical properties depend on the kind of metals.
- (2) Choose coexisting anions and their concentrations to control the relative adsorbabilities of metal anionic complexes on the resin.
- (3) Control the concentration of complexing agents, to adjust the stage of complex formation.

As for point (1), such complexing agents as fluoride, <sup>14,15</sup>) oxalate, <sup>11-13</sup>) and thiocyanate <sup>16-18</sup>) have been investigated. Fluoride has been most frequently adopted in the practical separations of hard acid-metals, probably because the stability constants of fluoride complexes depend on the kind of metals most strongly. Even in hydrofluoric acid (more than 0.1 M, 1 M=1 mol dm<sup>-3</sup>), however, sufficient separation is not expected unless other anions are present, since the difference in the adsorbabilities of fluoride complexes on a fluoride-form resin are not large enough. <sup>14</sup>)

As for point (2), such a mixed solvent as HF-HCl<sup>4-7</sup>) or HF-HNO<sub>3</sub><sup>8-10</sup>) has been proposed for the separation of hard acid-metals. The adsorbability of a chloride or nitrate ion on the anion exchange resin is much stronger than that of fluoride ion. With the strong adsorbability of chloride or nitrate, the relative adsorbabilities of metal fluoride complexes are weakened and the separation of hard acid-metals becomes possible.

As for point (3), Kraus et al.<sup>19)</sup> controlled the stage of chloride complex formation by adjusting the concentration of hydrochloric acid suitably and proposed the anion exchange separation of transition metals (including a few hard acid-metals).

If one would apply point (3) to the separation of

hard acid-metals in the media containing fluoride ions, the concentration of fluoride ion must be kept fairly low and constant, because these metals form fully fluorinated complexes such as  ${\rm ZrF_6}^{2-}$  and  ${\rm TiF_6}^{2-}$  in hydrofluoric acid more than 0.1 M. In solutions which contain fluoride ion in less than  $10^{-4}$  M, partially fluorinated complexes such as  ${\rm ZrF_5}^-$  and  ${\rm TiF_4}$  are expected to form.<sup>3)</sup>

In hydrofluoric acid solution or HF-HCl and HF-HNO<sub>3</sub> mixtures, however, it is not easy to maintain the fluoride ion concentration low and constant all through the procedures, since fluoride ions may be consumed by the relatively large amounts of metal ions or supplied from metal fluoride complexes adsorbed on the resin and fluoride-form resin.

The author reported in a previous paper<sup>3)</sup> that the fluoride ion concentration can be kept low  $(10^{-4} \text{ to } 10^{-5} \text{ M})$  in HF–H<sub>3</sub>BO<sub>3</sub> media according to the formation of fluoroboric acids, though the concentration of hydrofluoric acid is rather high (more than 0.1 M). In the media, the fluoride ion concentration is kept constant by the buffer action based on the dissociation of fluoroboric acids even when large amounts of metal ions are present.

In the present paper, the separation of hard acidmetals is discussed in HF-H<sub>3</sub>BO<sub>3</sub> media in relation to the above mentioned properties of HF-H<sub>3</sub>BO<sub>3</sub> media and the adsorbabilities of coexisting anions, while referring to points (2) and (3).

### **Experimental**

Chemicals and Apparatus. Standard solutions of metal ions were prepared by the procedures mentioned in the previous paper.<sup>3)</sup> Other chemicals and apparatus were also the same as used previously.

Ion Exchange Resin. A strongly basic anion exchange resin, Diaion SA \$\\$100, product of Mitsubishi Chemical Ind. Ltd. (8% DVB, 75 to 150  $\mu$ m, Cl<sup>-</sup>-form) was used. After washing the resin in a column with five times volume of 3 M HNO<sub>3</sub> and with distilled water until the effluent was free from nitrate ions, the resin was dried to constant weight at 70 °C and stored in a vacuum desiccator.

Determination of Distribution Coefficient. Method I: Fifty ml of a definite concentration of hydrofluoric-nitric acid solution or hydrofluoric-boric-nitric acid solution containing  $2 \times 10^{-4}$  M of a metal ion was added to a 150 ml polyethylene

bottle containing 0.5 g of the dried resin. The bottle was then shaken gently for 24 h at room temperature (the equilibrium is attained within 4 h). After filtration of the resin, the metal ion concentration in the solution was determined by a suitable method as previously described.<sup>3)</sup>

The distribution coefficient,  $K_d$ , was determined by the following equation:

 $K_d = (Amount of metal ion in resin/Amount of metal ion$ 

in solution)  $\times$  (ml of solution/g of resin) (ml/g)

Method II: Fifty ml of 0.2 M hydrofluoric acid solution containing  $2 \times 10^{-4}$  M of a metal ion was added to a 150 ml polyethylene bottle containing 0.5 g of the dried resin. The bottle was then shaken for 24 h at room temperature. After discarding the solution the resin was washed with 10 ml of  $10^{-2}$  M HF, and 50 ml of a definite concentration of HF–HNO<sub>3</sub> solution or HF–H<sub>3</sub>BO<sub>3</sub>–HNO<sub>3</sub> solution was added to the bottle. Subsequent procedures were the same as in Method I.

Column Operation. About 4 g of the dried resin in  $NO_3$ -form which had been swelled with distilled water was packed in a polyethylene column (8 mm $\phi$ ×180 mm) and the column was conditioned with about 50 ml of 0.2 M HF. After addition of a test solution containing 1 mg of a metal ion in 0.2 M HF, an eluent of a definite composition was passed through the column. The effluent was collected with a fraction collector and the concentration of the metal ion in each fraction was determined by the methods previously mentioned.<sup>3)</sup>

#### Results

The following experimental results were obtained in solutions containing more than  $10^{-2}$  M in HNO<sub>3</sub> in order to prevent the hydrolysis of hard acid-metals, unless otherwise mentioned.

Distribution Coefficients. Distribution coefficients  $K_d$  of Ti(IV), Zr(IV), Nb(V), and Ta(V) were investigated by Method I in solutions which contained various concentrations of hydrofluoric acid  $(C_{\rm HF})$  both in the presence and in the absence of 0.5 M  $H_3BO_3$ . The results are illustrated in Fig. 1.

The  $K_d$  values of these metals in HF-H<sub>3</sub>BO<sub>3</sub> media are smaller than those in HF. In both media, the  $K_d$  values of these metals are increased with the increase of  $C_{\rm HF}$  up to  $10^{-2}$  M. In solutions containing more than  $10^{-2}$  M of HF, the  $K_d$  in HF-H<sub>3</sub>BO<sub>3</sub> media are decreased with increasing  $C_{\rm HF}$ , whereas those in HF are almost unchanged with  $C_{\rm HF}$ . The  $K_d$  values in both media at any  $C_{\rm HF}$  decrease with increasing nitric acid concentration  $(C_{\rm HNO_3})$ .

The  $K_d$  values obtained by Method II are similar to those by Method I as shown in Fig. 2.

The  $K_d$  of other metals in HF-H<sub>3</sub>BO<sub>3</sub> media containing HNO<sub>3</sub> are presented in Table 1. In the third and fourth columns in Table 1,  $K_d$  in solutions containing various concentrations of H<sub>3</sub>BO<sub>3</sub> ( $C_{\rm H_3BO_3}$ ) and 0.1 M HF, and  $K_d$  in solutions containing various  $C_{\rm HF}$  and 0.5 M H<sub>3</sub>BO<sub>3</sub> are listed.

At constant  $C_{\rm HF}$  (column 3 in Table 1), the  $K_{\rm d}$  of W(VI), Nb(V), Hf(IV), Zr(IV), Mo(VI), Ti(IV), and Sn(IV) remarkably decrease when the  $C_{\rm H_3BO_3}$  is changed from  $10^{-2}$  to 0.1 M. The decrease of  $K_{\rm d}$  of Ta(V) with increasing  $C_{\rm HF}$ , however, is not noticeable.

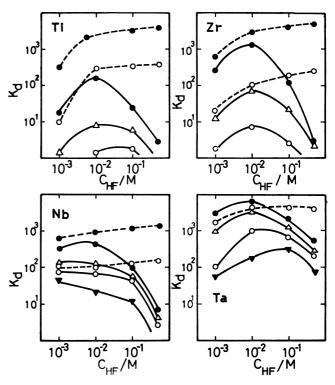


Fig. 1. Distribution coefficients of Ti(IV), Zr(IV), Nb-(V), and Ta(V) in HF and HF-H<sub>3</sub>BO<sub>3</sub> media containing HNO<sub>3</sub>.

HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-HNO<sub>3</sub> (----), HF-HNO<sub>3</sub> (-----).  $C_{\text{HNO}_3}$ ;  $\bullet$ :  $10^{-2}$  M,  $\triangle$ : 0.03 M,  $\bigcirc$ : 0.1 M,  $\blacktriangledown$ :

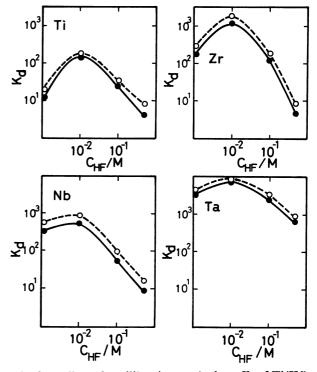


Fig. 2. Effect of equilibrating method on  $K_d$  of Ti(IV), Zr(IV), Nb(V), and Ta(V) in HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-10<sup>-2</sup> M HNO<sub>3</sub>.

---: Method I, --- Method II.

Table 1. Anion exchange distribution coefficients of metal ions in  $HF-H_3BO_3$  media containing  $HNO_3$ 

	0.1 M HF-H <sub>3</sub> BO <sub>3</sub>					HF-0.5 M H <sub>3</sub> BO <sub>3</sub>			
Ion [HNO <sub>3</sub> ]/M			$[H_3BO_3]/M$	[			[HF]/N		
	0	10-3	10-2	0.1	0.5	10-3	10-2	0.1	0.5
$Ta(V) \begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	>5×10 <sup>3</sup>	5×10 <sup>3</sup>	4.1×10 <sup>3</sup>	2.4×10 <sup>3</sup>	2.3×10 <sup>3</sup>	3.3×10 <sup>3</sup>	5×10 <sup>3</sup>	2.3×10 <sup>8</sup>	606
	$4.0\times10^3$	$1.5 \times 10^{3}$	$1.2 \times 10^3$	$1.0 \times 10^{3}$	790	102	955	790	315
$W(VI) \ \begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	$>$ 5 $\times$ 10 <sup>8</sup>	$5 \times 10^3$	765	97	232	$4.3\times10^3$	$2.4 \times 10^3$	232	13
	115	110	28	14	56	182	112	56	5
$Nb(V) = \begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	$5 \times 10^3$	$5.0 \times 10^3$	531	90	95	321	383	95	6
	102	91	68	18	58	79	71	58	3
Hf (IV) $\begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	$4.2 \times 10^3$	$2.2 \times 10^3$	$1.4 \times 10^3$	181	152	$1.0 \times 10^3$	$1.6 \times 10^3$	152	19
	360	320	245	7	<3	<3	10	<3	3
$Zr(IV)$ $\begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	$>$ 5 $\times$ 10 <sup>3</sup>	>5×10 <sup>3</sup>	$5.0 \times 10^3$	162	140	306	$1.3 \times 10^3$	140	4
	375	346	282	6	<3	<3	8	<3	<3
$\mathbf{Mo(VI)} \begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	$1.2 \times 10^3$	906	209	33	44	995	613	44	11
	75	56	25	4	15	48	33	15	6
(10-2	$>$ 5 $\times$ 10 <sup>3</sup>	$>$ 5 $\times$ 10 <sup>3</sup>	$3.8 \times 10^3$	70	15	18	150	15	3
$Ti(IV) \begin{cases} 10^{-1} \\ 10^{-1} \end{cases}$	405	355	302	18	<3	<3	<3	<3	<3
$(10^{-2})$	$>$ 5 $\times$ 10 <sup>3</sup>	$>$ 5 $\times$ 10 <sup>3</sup>	$5.0 \times 10^3$	57	15	39	141	15	14
$\operatorname{Sn}(\mathrm{IV}) \left\{ \begin{array}{l} 10 \\ 10^{-1} \end{array} \right.$	420	390	322	15	<3	<3	<3	<3	<3
$10^{-2}$	92	76	15	11		4	3	<3	<3
$V(V) = \begin{cases} 10^{-1} \\ 10^{-1} \end{cases}$	4	<3	<3	<3	<3	<3	<3	<3	<3
11/377 (10-2	72	49	5	<3	<3	20	15	<3	<3
$\mathbf{U}(\mathbf{VI}) \begin{cases} 10 \\ 10^{-1} \end{cases}$	<3	<3	<3	<3	<3 <3 <3 <3 <3	<3	<3	<pre> &lt;3 &lt;3 &lt;3 &lt;3 &lt;3 &lt;3 &lt;7</pre>	<3 <3 <3 <3 <3 <3 <3
10-2	12	6	13	15	<3	6	10	<3	<3
$\mathbf{V}(\mathbf{IV})  \begin{cases} 10 \\ 10^{-1} \end{cases}$	<3	<3	<3	<3	<3	<3	<3	<3	<3
Al(III) $\begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	30	20	12	10	7	8	5		3
	<3	<3	<3	<3	<3	<3	<3	<3	<3
$Cr(III)$ $\begin{cases} 10^{-2} \\ 10^{-1} \end{cases}$	31	28	14	<3	5	3	14	5	<3
	<3	<3	<3	<3	<3	<3	<3	5 <3	<3 <3
Fe(III), Cu(II), C Ni(II), Mn(II), C			<3				<3		

At constant  $C_{\rm H_3BO_3}$  (column 4 in Table 1), the  $K_{\rm d}$  of Hf(IV) or Sn(IV) is at a maximum when  $C_{\rm HF}$  is at around  $10^{-2}$  M, but the  $K_{\rm d}$  of W(VI) and Mo(VI) are large even when  $C_{\rm HF}$  is at  $10^{-3}$  M and decrease monotonously with the increase of  $C_{\rm HF}$ . This is similar to the results for Ti(IV), Zr(IV), Nb(V), and Ta(V) (Fig. 1). The large  $K_{\rm d}$  values of W(VI) and Mo(VI) at low  $C_{\rm HF}$  may be due to the fact that these metals exist as such anions as WO<sub>4</sub><sup>2-</sup> and Mo<sub>7</sub>O<sub>24</sub><sup>6-</sup> even in the absence of complexing agents.

The  $K_d$  of V(V), V(IV), U(VI), Al(III), Cr(III), and Fe(III) are small at most of  $C_{HF}$  and  $C_{HgBOg}$ .

According to the Ringbom's criterion for ion exchange separation by column filtration (i.e.  $K_d$  of an adsorbed ion is larger than  $10^2$  to  $10^{2.5}$  and that of the emerging ion is less than  $10^{0.5}$  to  $10^{1}$ ),  $^{20}$  the following results are expected from the  $K_d$  values in Fig. 1 and Table 1 for the column separation of hard acid-metals; (a) In 0.1 M HF- $10^{-2}$  M HNO<sub>3</sub>, hard acid-metals such as Ta(V), W(VI), Nb(V), Hf(IV), Zr(IV), Mo(VI), Ti(IV), Sn(IV), V(V), and U(VI) are retained in the column and V(IV) and Fe(III) are eluted from the column. Al(III) and Cr(III) are retained loosely or eluted slowly. (b) In 0.1 M HF-0.5 M  $H_3BO_3$ - $10^{-2}$  M HNO<sub>3</sub>, among the metals retained in the column in (a), V(V) and U(VI) are eluted and Ti(IV) and Sn(IV) are eluted slowly.

Mo(VI) is retained loosely. (c) In 0.1 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-0.1 M HNO<sub>3</sub>, among the metals retained in (b), Hf(IV) and Zr(IV) are eluted and Mo(VI) is eluted slowly. W(VI) and Nb(V) are retained loosely. (d) In 0.5 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-0.1 M HNO<sub>3</sub>, among the metals retained in (c), W(VI) and Nb(V) are eluted. Ta(V) cannot be eluted by the media mentioned above.

Although the media mentioned in (a) to (d) are chosen as an example, other possibilities for separation are obtained by selecting  $C_{HF}$ ,  $C_{H\circ BOO}$ , and  $C_{HNO}$ , properly.

are obtained by selecting  $C_{\rm HF}$ ,  $C_{\rm H_3BO_3}$ , and  $C_{\rm HNO_3}$  properly. Effect of Concentrations of HCl,  $H_2SO_4$ ,  $HNO_3$ , and HClO $_4$  on  $K_{\rm d}$  of Metals in HF- $H_3BO_3$  Media. The effects of various acids and their concentrations on the  $K_{\rm d}$  of Ti(IV), Zr(IV), Nb(V), and Ta(V) in  $10^{-2}$  M HF-0.5 M  $H_3BO_3$  are presented in Fig. 3. In this experiment the anion exchange resin used had been converted to the respective anion form, as in the coexisting acids (e.g. when coexisting acid is HClO $_4$ , the resin was converted to the ClO $_4$ --form).

Although the  $K_d$  values of all metals examined decrease with increasing the acid concentration regardless of the kind of acids, the degree of the effect of coexisting acids on  $K_d$  depends on the kind of acids; the effect is most serious with  $HClO_4$ .

The effect of concentration of sulfuric acid on  $K_d$  is gentle compared with those of other acids.

The  $K_d$  values of Nb(V) and Ta(V) are decreased

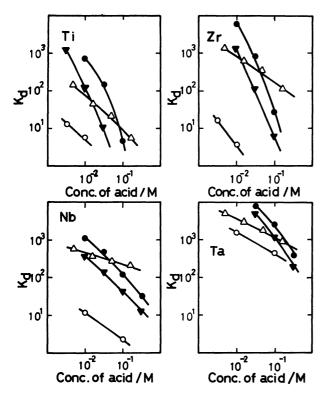


Fig. 3. Effect of concentration of coexisting acids on  $K_d$  of Ti(IV), Zr(IV), Nb(V), and Ta(V) in  $10^{-2}$  M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>.

lacktriangle: HCl,  $\triangle$ : H $_2$ SO $_4$ , lacktriangle: HNO $_3$ ,  $\bigcirc$ : HClO $_4$ .

more gently with the increase of acid concentration than those of Ti(IV) and Zr(IV).

Elution Behavior. In order to determine the practical conditions for the separation of Ti(IV), Zr(IV), Nb(V), and Ta(V), the elution behavior in  $HF-H_3BO_3$  media was investigated after adsorption of these metals in a column (4 g of the dried resin,  $8 \text{ mm}\phi \times 180 \text{ mm}$ ) in 0.2 M HF prior to the elution experiment. The flow rate of elution was adjusted to be 1.0 to 1.5 ml min<sup>-1</sup>. The elution curves are shown in integrated form in Fig. 4.

As expected from the  $K_d$  values obtained by the batch method (Fig. 1 and Table 1), the mutual separation of these metals is possible by the column method as follows.

Ti(IV) is eluted when 100 ml of  $10^{-2}$  M HF-0.5 M  $H_3BO_3$ - $3\times10^{-2}$  M HNO<sub>3</sub> or 0.1 M HF-0.5 M  $H_3BO_3$ - $10^{-2}$  M HNO<sub>3</sub> is passed through the column, while Zr(IV), Nb(V), and Ta(V) are retained in the column even with 400 ml of these eluents (Fig. 4, (a)). Ti(IV) and Zr(IV) are eluted with 100 ml of  $10^{-2}$  M HF-0.5 M  $H_3BO_3$ -0.1 M HNO<sub>3</sub> or 0.1 M HF-0.5 M  $H_3BO_3$ -0.1 M HNO<sub>3</sub>, and Nb(V) is eluted with 300 ml of these eluents (Fig. 4, (b)). Ti(IV), Zr(IV), and Nb(V) are eluted with 100 ml of 0.5 M HF-0.5 M  $H_3BO_3$ -0.1 M HNO<sub>3</sub>, while Ta(V) is not eluted with 300 ml of the eluent (Fig. 4, (c)). Ta(V) is eluted with 100 ml of 1 M HF-0.5 M  $H_3BO_3$ -5 M HNO<sub>3</sub> (Fig. 4, (d)-4), since the  $K_d$  value for Ta(V) in the medium is about 10.

The successive separation of Ti(IV), Zr(IV), Nb(V), and Ta(V) can be achieved when the media mentioned in (a) to (c) in Fig. 4 are properly combined as (d) in

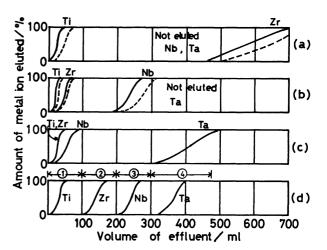


Fig. 4. Column elution behavior of Ti(IV), Zr(IV), Nb(V), and Ta(V) in HF-H<sub>3</sub>BO<sub>3</sub> media containing HNO<sub>3</sub>. Diaion SA \$\\$ 100: 4 g, flow rate: 1.0 ml/min. Concentration of HF-H<sub>3</sub>BO<sub>3</sub>-HNO<sub>3</sub> (M); (a)  $0.1-0.5-10^{-2}$  (——),  $10^{-2}-0.5-3\times10^{-2}$  (——),  $10^{-2}-0.5-0.1$  (——),  $10^{-2}-0.5-0.1$  (——),  $10^{-2}-0.5-0.1$  (c) 0.5-0.5-0.1, (d) ①:  $0.1-0.5-10^{-2}$ , ②: 0.1-0.5-0.1, ③: 0.5-0.5-0.1, ④: 1-0.5-5.

Fig. 4, as long as the amount of each metal is less than 1 mg.

Effect of Amount of Metal Ions on  $K_d$  and Elution Behavior of Metals. In HF-H<sub>3</sub>BO<sub>3</sub> media, the free fluoride ion concentration is extremely low, as mentioned in the previous paper.<sup>3)</sup> Therefore, the  $K_d$  values might be affected by the amount of metal ions owing to the deficiency of fluoride ions caused by the complex formation of large amount of metals with fluoride and/or the surplus of fluoride ions which are released from the large amount of metal fluoride complexes. This would occur especially when metals are adsorbed to the column in rather concentrated hydrofluoric acid in the beginning of the elution procedure.

The effect of the amount of Zr(IV) on  $K_d$  of Zr(IV) investigated by the batch method is summarized in Table 2. In this experiment, 2 g of the dried resin was used in order to keep the loading less than 0.1 and the solution of Zr(IV) was made free from fluoride ion. The  $C_{HF}$  was chosen so that the  $K_d$  of Zr(IV) is around  $10^2$  at 1 mg level of Zr(IV), i.e.  $10^{-3}$  M  $C_{HF}$  in the absence of  $H_3BO_3$  and 0.1 M  $C_{HF}$  in the presence of 0.5 M  $H_3BO_3$ .

The  $K_{\rm d}$  obtained by equilibrating the media containing Zr(IV) with the resin (Method I in Table 2) is decreased by the increase of the amount of Zr(IV) from 0.25 to 50 mg, when  $10^{-3}$  M HF- $10^{-2}$  M HNO<sub>3</sub> is used as the medium. But the  $K_{\rm d}$  is not changed with the amount of Zr(IV) up to 20 mg, when 0.1 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>- $10^{-2}$  M HNO<sub>3</sub> is used as the medium.

The  $K_d$  obtained by equilibrating zirconium-free media with the resin on which Zr(IV) had been adsorbed in 0.2 M HF (Method II in Table 2) is extremely large compared with that by Method I and is more than  $5\times10^3$  regardless of the amount of Zr(IV) when  $10^{-3}$  M HF– $10^{-2}$  M HNO<sub>3</sub> is used as the medium. On the other

Table 2. Effect of the amount of metal ions on distribution coefficients by	BATCH METHOD

T	Aı	mount	K <sub>d</sub>		
Ion	mg	mmol	Method Ia)	Method IIb)	
			(10 <sup>-3</sup> M HF–10 <sup>-2</sup> M HNO <sub>3</sub> )		
Zr(IV)	0.25	$2.7 \times 10^{-3}$	$1.0 \times 10^3$	$>5\times10^3$	
	1.0	$1.1 \times 10^{-2}$	90	$>5\times10^3$	
	10.0	0.11	6	$>5\times10^3$	
	50.0	0.53	3	$>5\times10^3$	
			(0.1 M HF-0.5 M H <sub>3</sub> BO <sub>3</sub> -10 <sup>-2</sup> M HNO <sub>3</sub>		
Zr(IV)	0.25	$2.7 \times 10^{-3}$	145	165	
, ,	1.0	$1.1 \times 10^{-2}$	142	160	
	10.0	0.11	132	168	
	20.0	0.21	126	162	
	50.0	0.53	42	155	
			(0.1 M HF-0.5 M	$H_3BO_3-0.1 M HNO_3$	
Nb(V)	1.0	$1.1 \times 10^{-2}$	65	68	
` '	10.0	0.11	66	82	
	20.0	0.22	70	75	

a) Determined by equilibrating the medium containing a metal ion with the resin. b) Determined by equilibrating the metal-free medium with the resin on which a metal ion had been adsorbed in 0.2 M HF.

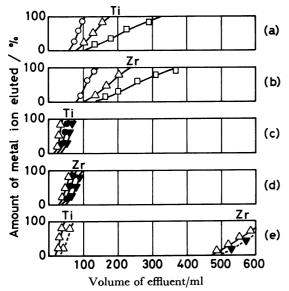


Fig. 5. Effect of amount of metal ions on elution behaviors of Ti(IV) and Zr(IV).

(a) and (b): 10<sup>-3</sup> M HF-0.1 M HNO<sub>3</sub>, (c) and (e): 0.1 M HF-0 5 M H<sub>3</sub>BO<sub>3</sub>-10<sup>-2</sup> M HNO<sub>3</sub>, (d): 0.1 M HF-0 5 M H<sub>3</sub>BO<sub>3</sub>-0.1 M HNO<sub>3</sub>. Amount of metal ions; ○: 0.25 mg, △: 1 mg, □: 5 mg, ●: 10 mg, ▼: 50 mg.

hand, when 0.1 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>- $10^{-2} \text{ M}$  HNO<sub>3</sub> is used as the medium, the  $K_{\rm d}$  by Method II is identical with that by Method I and is not affected by the amount of Zr(IV) up to 50 mg.

The reason why the  $K_d$  value in HF-H<sub>3</sub>BO<sub>3</sub>-HNO<sub>3</sub> media does not change may be attributed to the F-buffer action of this media, as mentioned in the previous paper.<sup>3)</sup>

The large  $K_d$  obtained by Method II in  $10^{-3}$  M HF–  $10^{-2}$  M HNO<sub>3</sub> cannot be explained clearly, but it may be due to the irreversible adsorption of Zr(IV)-fluoride complexes and/or the change of  $C_{HF}$  caused by the

partial dissociation of highly fluorinated zirconium complexes on the resin.

The  $K_d$  of Nb(V) in 0.1 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-0.1 M HNO<sub>3</sub> is the same regardless of the equilibrating method used and the amount of Nb(V), up to 20 mg.

The effect of the amount of Zr(IV) or Ti(IV) on their column elution behavior is shown in Fig. 5. These metals had been adsorbed to the column in 0.2 M HF prior to this elution experiment. Though the elution of Ti(IV) or Zr(IV) was extremely retarded by the increase of metal ions in 10<sup>-3</sup> M HF-0.1 M HNO<sub>3</sub> (Figs. 5(a) and (b)), the elution was hardly affected by increasing the amount of the metal ions up to 50 mg, when 0.1 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-0.1 M HNO<sub>3</sub> was used as the eluent (Figs. 5(c) and (d)). Less than 50 mg of coexisting Zr(IV) hardly affected the elution behavior of 1 mg of Ti(IV) in 0.1 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-10<sup>-2</sup> M HNO<sub>3</sub> (Fig. 5(e)).

## **Discussion**

The  $K_d$  values of metals for the anion exchange resin in solutions involving complexing agents are generally expressed by the equation presented by Helfferich.<sup>21)</sup> The equation can be modified into Eq. 1, by considering the adsorption of a metal ion  $M^{n+}$  to  $A^{a-}$ -form anion exchange resin in a solution containing fluoride ions as a complexing agent:

$$K_{\rm d} = \sum_{j=0}^{N} [x_j (K_{\rm A}^{\rm MF} j)^{1/a} ([{\rm A}^{a-}]_{\rm r}/[{\rm A}^{a-}])^{j-n/a}], \tag{1}$$

$$x_{j} = [F^{-}]^{j} \beta_{j} / (1 + [F^{-}] \beta_{1} + \dots + [F^{-}]^{N} \beta_{N}).$$
 (2)

Here j is the number of fluoride ions complexed with the metal ion  $M^{n+}$ , N is the maximum coordination number of fluoride ion for  $M^{n+}$ ,  $x_j$  is the molar fraction of  $MF_j$  to the total metal species in the solution,  $K_A^{MF_j}$  is the selectivity coefficient of  $MF_j$  to  $A^{a-}$ ,  $[A^{a-}]_r$  and  $[A^{a-}]$  are the concentration of anion  $A^{a-}$  in resin and solution and  $\beta_j$  is the cumulative stability constant of  $MF_j$ .

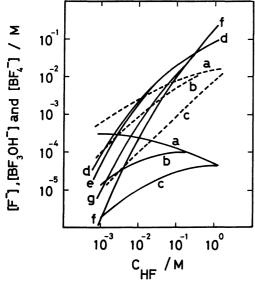


Fig. 6. Concentration of F<sup>-</sup>, BF<sub>3</sub>OH<sup>-</sup>, and BF<sub>4</sub><sup>-</sup> in HF and HF-H<sub>3</sub>BO<sub>3</sub> media containing HNO<sub>3</sub>.

——: HF-0.5 M H<sub>3</sub>BO<sub>3</sub>, -----: HF. a, b, and c: [F<sup>-</sup>] (a: without HNO<sub>3</sub>, b: with 10<sup>-2</sup> M HNO<sub>3</sub>, c: with 0.1 M HNO<sub>3</sub>), d and e: [BF<sub>3</sub>OH<sup>-</sup>] (d: without HNO<sub>3</sub>, e: with 0.1 M HNO<sub>3</sub>), f and g: [BF<sub>4</sub><sup>-</sup>] (f: without HNO<sub>3</sub>, g: with 0.1 M HNO<sub>3</sub>).

As is evident from Eq. 1, the  $K_d$  value is a function of  $x_j$ , which is controlled by  $[F^-]$  in the solution (Eq. 2), of  $(K_A^{MF})^{1/a}$  which indicates the relative adsorbability of  $MF_j$  to  $A^{a-}$  (and hence, the value depends on the kind of anion), and of  $([A^{a-}]_r/[A^{a-}])^{r-n/a}$ , which depends on the valency and the concentration of anion  $A^{a-}$ .

Concentrations of free fluoride ion and other anions which exist in hydrofluoric acid and HF-H<sub>3</sub>BO<sub>3</sub> media containing HNO<sub>3</sub> are calculated by the procedure described in the previous paper.<sup>3)</sup> These are illustrated in Fig. 6; the dissociation constants of hydrofluoric acid and fluoroboric acids were used.

Figur 6 and the dependency of  $K_{\rm d}$  on  $C_{\rm HF}$  shown in Fig. 1 can be explained as follows: In solutions containing less than  $10^{-2}$  M HF and  $10^{-2}$  M HNO<sub>3</sub> with and without 0.5 M H<sub>3</sub>BO<sub>3</sub>, the resin stays as NO<sub>3</sub>—form because the concentration of anions in solution other than nitrate is low and, hence, the second and third terms in Eq. 1 can be considered as constant at a definite  $C_{\rm HNO_3}$ . Therefore, the increase of  $K_{\rm d}$  with increasing  $C_{\rm HF}$  up to  $10^{-2}$  M may be ascribed to the change of  $x_{\rm j}$  term, that is, to the increase of anionic metal fluoride complexes.

As an example, the species of Zr(IV) fluoride complexes and their fractions  $x_j$  in  $HF-H_3BO_3$  media are calculated using the stability constants of Zr(IV) fluoride complexes.<sup>22)</sup> The free fluoride ion concentration in the media of 0.5 M  $H_3BO_3-10^{-2}$  M HNO<sub>3</sub> containing  $10^{-3}$  or  $10^{-2}$  M HF is  $10^{-5.0}$  or  $10^{-4.3}$  M, respectively (see Fig. 6). The molar fraction of major species of Zr(IV) in solutions containing  $10^{-5.0}$  M or  $10^{-4.3}$  M of free fluoride ion are 35% of  $ZrF_4$ , 15% of  $ZrF_5$ , and 2% of  $ZrF_6^{2-}$  or 30% of  $ZrF_4$ , 55% of  $ZrF_5$ , and 15% of  $ZrF_6^{2-}$ , respectively. Consequently, the increase of the  $K_d$  of Zr(IV) with increasing  $C_{HF}$ 

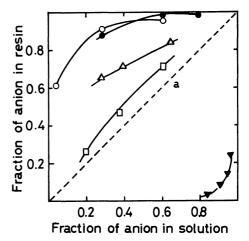


Fig. 7. Exchange of anions with Cl<sup>-</sup> in the resin.
Diaion SA # 100: 1.0 g. Amount of acids: 0.5 to 20 mmol in 20 ml of solution. ○: BF<sub>4</sub><sup>-</sup>, ●: ClO<sub>4</sub><sup>-</sup>, △: NO<sub>3</sub><sup>-</sup>, □: SO<sub>4</sub><sup>2-</sup>, ▼: F<sup>-</sup>.

is mainly due to the increase of the fraction of  $ZrF_5^-$  (and  $ZrF_6^{2-}$ ).

The decrease of  $K_{\rm d}$  with the increase of  $C_{\rm HF}$  in HF-H<sub>3</sub>BO<sub>3</sub> media containing more than  $10^{-2}$  M HF (see Fig. 1) cannot be explained by the change of  $x_j$  because the free fluoride ion concentration slightly increases with the increase of  $C_{\rm HF}$  (Fig. 6), but may be attributed to the change of the second and third terms in Eq. 1. Because the concentration of BF<sub>4</sub><sup>-</sup> and BF<sub>3</sub>OH<sup>-</sup> increases remarkably with increasing  $C_{\rm HF}$  in the solutions which are more than  $10^{-2}$  M HF and 0.5 M H<sub>3</sub>BO<sub>3</sub> (Fig. 6), it is suspected that BF<sub>4</sub><sup>-</sup> and BF<sub>3</sub>OH<sup>-</sup> are adsorbed rather strongly on the resin, reducing the relative adsorbabilities of the metal fluoride complexes.

The adsorbability of BF<sub>4</sub>- was investigated and compared with the adsorbabilities of ClO<sub>4</sub><sup>-</sup>, NO<sub>3</sub><sup>-</sup>, SO<sub>4</sub><sup>2</sup><sup>-</sup>, and F<sup>-</sup> according to Wheaton *et al.*<sup>23)</sup> After equilibrating 1.0 g of Cl--form dry anion exchange resin with 20 ml of various concentrations of HBF<sub>4</sub>, HClO<sub>4</sub>, HNO<sub>3</sub>, H<sub>2</sub>SO<sub>4</sub>, or HF for 24 h at room temperature, the amount of chloride ion desorbed from the resin was determined by the Volhard method.<sup>24)</sup> Assuming the amount of chloride desorbed is equivalent to the anions adsorbed, the molar fractions of the anion examined both in resin and solution are calculated (Fig. 7). In Fig. 7, the curve of an anion which lies above line (a) suggests the stronger adsorbability of the anion than that of chloride ion.<sup>23)</sup> It is seen from Fig. 7 that the adsorbability of BF<sub>4</sub>- is very strong and is comparable to that of ClO<sub>4</sub>-. The order of adsorbabilities of anions is as follows:

$$BF_4^- \simeq ClO_4^- > NO_3^- > SO_4^{2-} > Cl^- > F^-.$$
 (3)

Although the adsorbability of BF<sub>3</sub>OH<sup>-</sup> cannot be determined experimentally because of the difficulty of the preparation of BF<sub>3</sub>OH<sup>-</sup> free from BF<sub>4</sub><sup>-</sup>,<sup>25)</sup> it is considered that BF<sub>3</sub>OH<sup>-</sup> has the similar adsorbability to that of BF<sub>4</sub><sup>-</sup> since the structure and the ionic charge of BF<sub>3</sub>OH<sup>-</sup> resemble those of BF<sub>4</sub><sup>-.25)</sup>

According to the considerations mentioned above, the decrease of  $K_d$  with the increase of  $C_{\rm HF}$  in HF-H<sub>3</sub>BO<sub>3</sub> media containing more than  $10^{-2}$  M HF (Fig. 1) may

be attributed to the increase of  $BF_4^-$  and  $BF_3OH^-$  which are strongly adsorbed on the resin. And the decrease of  $K_d$  with the increase of  $C_{H_3BO_3}$  in  $HF-H_3BO_3$  media containing more than  $10^{-2}$  M  $H_3BO_3$  (column 3 in Table 1) may also be attributed to the increase of  $BF_4^-$  and  $BF_3OH^-$ .

The effects of coexisting acids and their concentrations on  $K_d$  (Fig. 3) may also be due to the difference in the adsorbabilities of the anions included in the coexisting acids. The different adsorbability given by various kinds of anions changes the second term in Eq. 1,  $(K_{\Lambda}^{MFj})^{1/a}$ , and the concentrations of anions affect the third term in Eq. 1,  $([A^{a-}]_r/[A^{a-}])^{j-n/a}$ .

Based on the above discussions, the separation of Ti(IV), Zr(IV), Nb(V), and Ta(V) in HF-H<sub>3</sub>BO<sub>3</sub> media shown in Fig. 4(d) is interpreted as follows: Metals in 0.2 M HF are adsorbed on the resin as fully fluorinated complexes. When the eluent,  $0.1~M~HF-0.5~M~H_3BO_3-10^{-2}~M~HNO_3$ , is introduced to the column, metal complexes tend to be transformed to partially fluorinated complexes and the  $K_d$  values of these metals are reduced, because the concentration of free fluoride is extremely low in the medium. With this eluent Ti(IV), whose  $K_d$  is the smallest among these metals in this medium, is eluted from the column. With the increase of  $C_{\text{HNO}_3}$  in the eluent, the amount of NO<sub>3</sub>- adsorbed on the resin is increased, and Zr(IV) is eluted. When  $C_{\rm HF}$  is increased from 0.1 M to 0.5 M, BF<sub>4</sub>- or BF<sub>3</sub>OH-, whose adsorbabilities are stronger than that of NO<sub>3</sub>-, is increased and Nb(V) is eluted. Since the adsorbability of Ta(V) fluoride complexes is extremely strong, a medium containing strong adsorptive anions in rather high concentration such as 1 M HF-0.5 M H<sub>3</sub>BO<sub>3</sub>-5 M HNO<sub>3</sub> is required to elute Ta(V).

Generally, in the separation of hard acid-metals by anion exchange, mixtures of HF (more than 0.1 M) and fairly concentrated HCl<sup>4-7</sup>) or HNO<sub>3</sub><sup>10</sup>) are used as eluents. Using these media, however, a separation such as that of Ti(IV) from Zr(IV) is difficult, because the adsorbabilities of fully fluorinated complexes of these metals resemble each other. Although for the elution of Ta(V) a solution of salt in high concentration such as 1 M NH<sub>4</sub>F-4 M NH<sub>4</sub>Cl<sup>4,7</sup>) or a mixture of concentrated acids such as 5 M HF-12 M HNO<sub>3</sub><sup>10</sup>) are employed in the works of HF-HCl or HF-HNO<sub>3</sub> media, it is difficult to remove the large amount of salts from the effluent and the concentrated acids decompose the resin. Using HF-H<sub>3</sub>BO<sub>3</sub> media proposed in the present paper, these disadvantages are eliminated.

In conclusion, there is a buffer action relating to fluoride ion based on the dissociation of fluoroboric acids in HF-H<sub>3</sub>BO<sub>3</sub> media, as discussed in the previous paper.<sup>3)</sup> Therefore, despite the low fluoride ion concentration in HF-H<sub>3</sub>BO<sub>3</sub> media, the separation can be

attained without any effect of the amount of metal ions (up to 50 mg) as illustrated in Table 2 and Fig. 5.

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